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A) $R = 1 \text{ pc}$ $T = 30, 100 \text{ K}$
 $n = 10^{10} / \text{m}^3$ $\text{AND } \text{H}_2 \rightarrow \mu = 2$

TOTAL MASS OF CORE: $M = \frac{4}{3} \pi R^3 \rho$ $M = \frac{4}{3} \pi (3.09 \times 10^6 \text{ m}) (3.34 \times 10^{-17} \frac{\text{kg}}{\text{m}^3})$

WHERE $\rho = 2 m_{\text{H}} n$

$M \approx 4 \times 10^{33} \text{ kg} \approx \boxed{2000 M_{\odot}}$

$R_{\text{JEAN}} = \left(\frac{15 kT}{4 \pi G \mu m_{\text{H}} \rho} \right)^{1/2} = \left[\frac{15 (1.38 \times 10^{-23} \frac{\text{J}}{\text{K}}) (30 \text{ K})}{4 \pi (6.67 \times 10^{-11}) (2) (1.67 \times 10^{-27} \text{ kg}) (3.34 \times 10^{-17} \frac{\text{kg}}{\text{m}^3})} \right]^{1/2}$

$R_{\text{JEAN}, 30\text{K}} = 8.15 \times 10^{15} \text{ m} = \underline{0.26 \text{ pc}}$

$R_{\text{JEAN}, 100\text{K}} = 1.49 \times 10^{16} \text{ m} = \underline{0.48 \text{ pc}}$

SINCE THE CORE MASS IS $\sim 2000 M_{\odot}$, AND THE JEANS LENGTH TO COLLAPSE IS SIMILAR TO THE CORES $\sim 1 \text{ pc}$ SIZE, THEN WHAT COLLAPSES WILL NOT BE A $1 M_{\odot}$ STAR. IT WILL BE MUCH LARGER.

B) THE SAME METHOD AS IN PART A) IS USED

MASS OF KNOT $\approx 200 M_{\odot}$

$R_{\text{JEAN}, 30\text{K}} = 0.03 \text{ pc}$

$R_{\text{JEAN}, 200\text{K}} \approx 0.07 \text{ pc}$

THE SUB-PART OF THE KNOT THAT WILL BE COLLAPSING WILL BE IN THE GENERAL RANGE OF STELLAR MASSES

c) CASE B] IS THE MORE LIKELY CASE

$$t_{\text{ff}} = \sqrt{\frac{3\pi}{32 G \rho}} = \left[\frac{3\pi}{32 (6.67 \times 10^{-11}) (3.34 \times 10^{-15} \frac{\text{kg}}{\text{m}^3})} \right]^{\frac{1}{2}} = 1.15 \times 10^{12} \text{ s} = 35,000$$

35,000 YEARS

d) INITIALLY, U IS SMALL, BUT IT BECOMES LARGE SINCE $T \rightarrow 3000\text{K}$

FROM THE VIRIAL THEOREM, $E = -U$, SO $|E| = |U|$. IF WE FIND

U_{FINAL} , WE CAN THEN KNOW THE E EMITTED, TOO.

$$U = \frac{3}{2} \frac{M}{\mu m_{\text{H}}} kT, \quad M = 200 M_{\odot}$$

$$U = \frac{3}{2} \frac{4 \times 10^{32} \text{ kg}}{(2)(1.67 \times 10^{-27})} (1.38 \times 10^{-23})(3000) = 7.4 \times 10^{39} \text{ J}$$

$$L = \frac{\Delta E}{\Delta t} = \frac{E}{t_{\text{ff}}} = \frac{|U|}{t_{\text{ff}}} = 6.5 \times 10^{27} \frac{\text{J}}{\text{s}} \approx 17 L_{\odot}$$

AT IR WAVELENGTHS

$$e) \frac{\Omega_{\text{GRV}}}{\text{VOL}} = \frac{-\frac{3}{5} \frac{GM^2}{R}}{\frac{4}{3}\pi R^3} = 0.6 \frac{(6.67 \times 10^{-11})(4 \times 10^{32})^2}{(3.086 \times 10^{15} \text{ m})} = \frac{2.07 \times 10^{39}}{1.23 \times 10^{47}} = 1.68 \times 10^{-8} \frac{\text{J}}{\text{m}^3}$$

$$E_{\text{DENSITY B-RKD}} = \frac{1}{2\mu_0} B^2 = 1.68 \times 10^{-8} \frac{\text{J}}{\text{m}^3}$$

$$B = \left[(1.68 \times 10^{-8})(2)(4\pi \times 10^{-7}) \right]^{\frac{1}{2}}$$

$$B = 2.05 \times 10^{-7} \text{ TESLA}$$

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2.2 - TEXTBOOK

$$1) M_J = \frac{4}{3} \pi \rho R_J^3$$

 $b \geq 1$ BY DEFINITION

$$\frac{1}{\alpha} M_J = \frac{4}{3} \pi \rho \left(\frac{R_J}{b}\right)^3$$

$$\frac{1}{\alpha} M_J = \frac{4}{3} \pi \rho R_J^3 \frac{1}{b^3}$$

$$b^3 = \alpha \implies b^3 \geq \alpha \text{ FOR COLLAPSE}$$

2) $TV^{\gamma-1} = \text{CONSTANT}$ FOR AN ADIABATIC PROCESS

$$T \left(\frac{1}{\rho}\right)^{\gamma-1} = \text{CONSTANT}$$

$$T_I \left(\frac{1}{\rho_I}\right)^{\gamma-1} = T_F \left(\frac{1}{\rho_F b^3}\right)^{\gamma-1}$$

$$\gamma - 1 = \frac{5}{3} - 1 = \frac{2}{3}$$

$$T_I \rho_I^{-2/3} = T_F \rho_F^{-2/3} b^{-2}$$

$$T_F = T_I b^2$$

$$M_J \propto T^{3/2} \quad \text{SO THAT} \quad \text{(Eq. 2.16)}$$

$$M_J \propto b^3$$

THE JEANS MASS GOES UP

$$1) \mu_{\text{INIT}} = 1.3 \quad \frac{\mu_I}{\mu_{\text{FINAL}}} = \frac{13}{6}$$

$$\mu_{\text{FINAL}} = 0.6$$

INITIAL: $R_{J,I} = \left(\frac{15 kT}{4 \pi G \mu m_H \rho}\right)^{1/2} = \frac{X^{1/2}}{\mu_I^{1/2} \rho^{1/2}}$

FINAL: $\frac{R_J}{b} = \frac{X^{1/2}}{\mu_F^{1/2} (\rho b^3)^{1/2}} \implies R_J = \frac{X^{1/2}}{\mu_F^{1/2} (\rho b^3)^{1/2}} \cdot b$

COMPRESSION AFFECTS DENSITY AS WELL

$$b = \frac{36}{169} = 0.21$$

2.2

c) CONTINUED:

$$\frac{\cancel{\chi}^{1/2}}{\mu_1^{1/2} \rho^{1/2}} = \frac{\cancel{\chi}^{1/2} b}{\mu_F^{1/2} \rho^{1/2}} b^{-3/2}$$

$$\left(\frac{\mu_F}{\mu_1}\right)^{1/2} = b^{-1/2}$$

$$\left[\left(\frac{16}{13}\right)^{1/2}\right]^{-2} = \boxed{b = 2.17}$$

d) $L_I \propto R_I^2 T_I^4$

$T\left(\frac{1}{\rho}\right)^{\delta-1} = \text{const. AND FROM b) } \underline{T_F = T_I b^2}$

$$L_F \propto \left(\frac{1}{b} R_I\right)^2 (b^2 T_I)^4$$

$$\frac{L_F}{L_I} = \left(\frac{1}{b}\right)^2 (b^2)^4 = \boxed{\frac{L_F}{L_I} = b^6}$$

THE CLOUD WOULD BE ABLE TO RADIATE ENERGY AWAY VERY EFFICIENTLY, WHICH WILL AID IN COLLAPSE

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PRESSURE SUPPORT vs. GRAVITY

A) $\frac{dp}{dr}$ vs. $\frac{-GM\rho}{r^2}$

ASSUME ISOTHERMAL, UNIFORM CONTRACTION

(IDEAL GAS)

$$\frac{dp}{dr} \sim \frac{p}{r} \sim \frac{p k T}{r} \sim \frac{n^3}{r} \sim \boxed{n^2}$$

$$\frac{-GM\rho}{r^2} \sim \frac{n^3}{r^2} \sim \boxed{r}$$

$$\text{RATIO} = \frac{\frac{dp}{dr}}{\frac{-GM\rho}{r^2}} \sim \frac{n^2}{r} \sim \boxed{r}$$

AS $r \rightarrow 0$, THE RATIO OF THESE TWO TERMS ALSO GOES TO ZERO, MEANING THAT THE PRESSURE SUPPORT WILL BECOME EVEN WEAKER AS THE CLOUD COLLAPSES.

B) now $\frac{dp}{dr} \sim \frac{p}{r} \sim \frac{p k T}{r} \sim \frac{n^3 r^{-q}}{r} \sim n^2 r^{-q-1}$

$$\text{RATIO} = \frac{\frac{dp}{dr}}{\frac{-GM\rho}{r^2}} \sim \frac{n^2 r^{-q-1}}{r} \sim n r^{-q}$$

IF $q > 1$ THEN AS $r \rightarrow 0$, THE RATIO WOULD INCREASE WHICH WOULD HELP TO STOP THE COLLAPSE. SO IF $T \propto r^{-1}$ (OR UNLESS), FREE-FALL CONTRACTION WOULD BE HALTED.